

**BRIDGwall v2 – CHBDC and AASHTO
Abutment and Retaining Wall Design
User's Manual**

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1.0 INSTALLATION

1.1 Hardware Requirements

To successfully install BRIDGwall, your computer must be equipped with the minimum:

- Windows 10 or later operating system
- P2 processor
- 64 MB of Ram
- 2 MB of free disk space
- 800 x 600 video
- Microsoft Excel 2010 (Excel 2007 not recommended)

1.2 Installation and Uninstall Program

BRIDGwall is equipped with an automatic installation program.

- The program is run and installed directly from our website. The package includes the Excel workbooks required as the starting point of your first new design. Later designs may utilize these workbooks or other saved workbooks generated from the original Excel file.
- The application as received will require registration to enable full design functionality. The program will operate in demo until registered.
- The Excel files contain macros. The User will need to accept the macros in order to enable the program functionality.
- An Uninstall routine will be installed in the same directory as the program directory. The program may be uninstalled and then reinstalled during an active license without issue.
- Your system requires Microsoft .NET Framework (included in Windows 7 and later) to operate the BRIDGwall program. During the BRIDGwall installation, your system may automatically be directed to the Windows download website to retrieve the necessary file.
- After installation, the program will automatically check for the latest program version when the application is re-opened.

2.0 DEFINITIONS

For definitions, see the applicable section of the Canadian Highway Bridge Design Code (CHBDC) CAN/CSA-S6-19 or the American Association of State Highway and Transportation Officials (AASHTO).

3.0 NOTATION

For notations, see the applicable section of CHBDC or AASHTO and as follows:

DC – dead load of structural component and non-structural attachments
EH – horizontal earth pressure
EQ – earthquake
ES – earth surcharge load
EV – vertical pressure from dead load of earth fill
F_h – horizontal force
F_v – vertical force
F_{h_x} – horizontal force along X axis
F_{h_y} – horizontal force along Y axis
H_x – horizontal force in X direction
H_y – horizontal force in Y direction
K_a, K_{ah}, K_o, K_{oh} – earth pressure coefficients
LH – horizontal force from live surcharge
LL – vehicular live load
LV – vertical load from live surcharge
Pa – soil force
Pa_h – horizontal soil force
Pa_y – soil force along Y axis
P_{H_x} – horizontal forces along the X axis
P_{H_y} – horizontal forces along the Y axis
Ph_y – horizontal component of *Pa_y*
P_{oh}, P_{oh_y} – horizontal force from resisting soil
P_{V_y} – vertical component of *Pa_y*
M_{h_x} – moment about the Y axis or in the X axis direction
N/A – not applicable
p – horizontal distance from the front face of abutment at bearing seat level
WA – water load
X axis – direction parallel to wall face
Y axis – direction perpendicular to wall face

4.0 INTRODUCTION

4.1 General

BRIDGwall by Simplified Bridge Solutions Ltd. is a program that provides abutment and retaining wall (including gravity walls) conforming to CHBDC and AASHTO, herein after referred to as 'the bridge codes' or 'the codes'. The intent of this program is to provide a user-friendly tool for many of the earth retaining structures being designed today.

As most of the User information is contained in the bridge codes, the User should refer primarily to the codes more so than the BRIDGwall manual when using the program. Therefore, references to clauses, sections, tables and figures shall be that of the codes unless noted otherwise.

4.2 Description

BRIDGwall is a program that uses Microsoft Excel (output) and Visual Basic (input) for designing abutments, retaining walls, and gravity walls.

BRIDGretainingwall and BRIDGabutment complete the available Excel files to the BRIDGwall program.

BRIDGretainingwall is very similar to BRIDGabutment with the exception that a footing key may be modeled, a water table may be entered on the retained backfill side, and rotation of gravity walls is available.

BRIDGabutment allows forces to be entered at the bearing seat location and includes input for a ballast wall.

5.0 INPUT

5.1 General

For BRIDGabutment, a bridge structure may first be modeled using our BRIDGframe program to obtain the forces at the bearings

To begin using the BRIDGwall program, the User is required to LOAD (see the LOAD buttons found on file tab of the program) the BRIDGabutment or BRIDGretainingwall model into BRIDGwall. See Appendix 3.

Input data is posted to the various Excel worksheets to be utilized by the program, by the selection of the 'Synchronize' button.

The program uses fixed units of measurement in the international or metric system.

5.1.1 Sign Convention

The program will only allow positive or negative values as dictated by the program. If an incorrect value (positive or negative) is enter, an error message pops up saying the value is INVALID.

Generally, positive vertical forces act downwards, positive horizontal forces contribute to overturning, and positive transverse moments increase the soil bearing pressure. See Appendix 4.

5.2 Properties

The Properties tab provides for the property and parameter input of the resisting and retained backfill, and the founding material.

Angle of Wall Friction (BRIDGabutment and BRIDGretainingwall) and Wall Rotation (BRIDGretainingwall) is applicable to Gravity Walls only and must me left bank when designing a cantilever style wall. Angle of Wall Friction is a mandatory input requirement for gravity type walls.

For abutment design, Road Top to Abutment Top is included as an input value. The program **does not** use this information to calculate the backfill surcharge load at the top of the abutment; but uses this information to determine the amount of compaction surcharge (CHBDC only) at the top of abutment wall only. This input is typical for semi-integral abutment bridges.

The Height of Water Table is measured vertically from the end of the footing toe. The height of water table is applied to the Retained Backfill side only. Hydrostatic uplift is assumed to act linearly from the end of heel (maximum uplift pressure) to the end of toe (minimum uplift pressure = 0).

The starting point for the sloped retained backfill is at the top corner of the wall on the retained soil side.

To eliminate sliding as part of the 'Optimization' (Geometry tab) of the footing, the 'Effective Friction Angle' and 'Effective Friction Angle at u/s of Footing' may to set to 45 ° on the Properties tab or cohesion can be added even if not a condition. This may

be applicable when footings are keyed into bedrock or dowels are provided between the footing and bedrock.

5.3 Loads

5.3.1 Loads 1

The Loads 1 tab is used to input the General Loads of, surcharges, lateral seismic uniform pressure on the retained soil side (provided by Geotechnical Engineer), along with identifying the use of approach slabs and the density of the structure. General Loads are applicable to both BRIDGretainingwall and BRIDGabutment. As per the code, earthquake or seismic loads are not applied with live loads. As such, BRIDGwall will only allow one of these loads to be entered at any one time.

Amplification of soil pressure due to earthquake load is applied as an additional uniform soil pressure.

'Permanent UDL Surcharge' requires completion regardless of if 'Road Top to Abutment Top' was completed on the Properties tab.

Loads 1 also provides for Additional Horizontal/Overturning Loads for BRIDGretainingwall.

5.3.2 Loads 2

Loads on the Bearing Seat is available to BRIDGabutment and provides for the input of forces on the bearing seat. These loads are assumed to act through the centroid of the abutment in the X direction and at a distance "p" from the front face of the abutment wall.

As per cl.3.5.2.2 (CHBDC), minimum Dead & SIDL's should use a load factor of 1.0 when establishing F_v and M_{hx} using F_v .

5.3.3 Loads 3

The Loads 3 tab is used to input the Load Factors, typically at ULS (CHBDC) or Strength (AASHTO).

The resisting soil pressure calculated by the program is that of At-rest Earth Pressure rather than that of Passive Earth Pressure. An input load factor box for SLS (CHBDC) or Service (AASHTO) horizontal earth pressure has been provided so the User may increase the horizontal resisting soil pressure from At-rest up to that of Passive. Likewise, the User can modify the ULS or Strength maximum and minimum horizontal load factors to obtain Passive resistance instead of At-rest resistance.

Default values are automatically loaded for the applicable code when the code is selected on the File tab. To change the load factor values back to the original defaults, if changes were made, a Get Defaults button is provided.

Note: For the two values of LH on the Loads 3 tab, the default value has been set to 1.7 as per C6.12.5. However, MTO is still using 1.25 for these values so the User may decide to overwrite the default values.

As per cl.3.5.2.2 (CHBDC), the vertical loads are defaulted to 1.0.

5.4 Geometry

The Geometry tab is used to establish the dimensional properties of the wall structure.

Input varies somewhat depending on whether a BRIDGabutment or BRIDGretainingwalll file was loaded.

If a Gravity Wall is being modeled (see 5.2 Properties), the Heel Width will not be available for input.

For Gravity Walls with no footings, use a very small footing depth such as 0.0001 m to remove the warning message on the Geometry tab.

A dynamic cross section of the wall structure is provided at scale to assist in verifying the input values.

An Optimize button is provided to allow the User to determine the smallest possible overall footing size, or the smallest heel size using a designation toe width, or the smallest toe size using a designated heel width.

A value greater than zero shall be entered for the Heel Width of Cantilevered Walls when using the Optimize option.

The length of the footing should be set equal to the length of the abutment or just slightly larger at most. Additional fill on the abutment footing that extends beyond the abutment wall length is not considered in design. The length of footing is only used for calculating bearing resistance as per cl.6.10.2 (CHBDC).

5.5 Design

A Rebar Design tool and a Pile Foundation design tool have been provided to assist the User in completing the design of the wall structure.

For pile foundation design, the plan geometry of the piles is input, and the remaining design focuses on a single pile as chosen by the User.

Input of the forces obtained from the worksheets, is done through the program on the Design tab. Additional input is done directly in the Excel workbooks. See Example 3 in Appendix 6.

6.0 OUTPUT

6.1 General

References to CHBDC or AASHTO are provided on each output sheet to assist the User in verifying the application.

Serviceability and Strength conditions are addressed.

6.2 Results

The output consists of typical combinations using varying maximum and minimum load combinations. It is unlikely some combinations will ever govern design; however, they are shown for information purposes only. It is assumed the User may only wish to print the governing worksheet, so service conditions which may be the same on all worksheets, is provided on all worksheets.

A summary of the results for soil bearing, sliding, overturning, and resultant location, is provided at the bottom of the Input worksheet.

If a water table was input, the program does not automatically check if the worst condition is without a water table.

6.2.1 Geotechnical Analysis

The Info contained on the Geo 1 to Geo 4 worksheet contains the analysis of the various load combinations for the allowable bearing pressure on the founding material.

The Geo 5 worksheet contains the analysis of eccentricity limits, overturning and sliding resistance.

6.2.2 Structural Analysis

The Info contained on the Str 1 to Str 4 worksheet contains the analysis of the various load combinations for the structural forces in the wall, toe and heel components which make up the structure.

6.2.3 Design 1

The Design 1 worksheet shows the structural design of the chosen component. Design includes service stresses and strength design for rebar reinforced concrete, for moment and shear design.

6.2.4 Design 2

The Design 2 worksheet shows the properties of the pile group configuration, and the design results of a single User selected pile.

Structural design includes the axial force in the selected pile and a structural axial capacity work area. For a structure requiring passive resistance against the pile to

satisfy horizontal displacement of the structure, a more rigorous design may be required to account for bending moments and shear.

6.2.5 Helical Piles

A helical pile worksheet is included. It allows for a single batter in piles only. All Str worksheets are checked at the same time. Design includes compression and tension piles.

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7.0 Printing

Printing of Excel sheets is done by selection of each worksheet as found on the program 'Print' sheet. Printing may also be done manually by selecting the data of interest and designating it for printing using the Print Area command.

To print the program input sheets (tab dialogue pages), the User may press 'Ctrl,' 'Alt' and 'Prt Sc' simultaneously when on the sheet of preference to print; then in Microsoft Word place the cursor where the top left corner of the saved print screen will be dropped and press 'Ctrl' and 'V' simultaneously.

8.0 Troubleshooting

If the User does not Load a compatible Excel file, an Error or Error message will appear. Probable Resolution: Load a compatible Excel BRIDGabutment or BRIDGretainingwall spreadsheet that was received with the program.

The program fails during registration confirmation. Probable Resolution: The firewall may be blocking communication with our website. Configure the firewall to allow communication with www.bridge-structural.com. Confirm there is an internet connection. Further configuration of the firewall may be required to allow BRIDGwall.exe and BRIDGwallUpdater.exe to access the internet.

If the appearance of the program is not as per the screen prints shown in the Appendix 4 Input Examples, the issue may be with the monitor settings. Right click on the Desk Top, select Properties/ Settings/ Advanced/ General Tab/ the DPI setting should be that of Normal Setting.

The program fails and gives an error message when trying to analyze. Probable Resolution: Macros have not been allowed to run. Excel 2007 and later require special attention to have Trust settings configured to allow macros within BRIDGwall to run.

Computer Regional Settings must be set for English. See also www.support.microsoft.com/kb/320369

Error Number 5 Access to the path 'C:\ProgramFiles(x86)\Simplified Bridge Solutions\BRIDGframe\SBS.ini' is denied. Probable Resolution: writing permission is required to C:\ProgramFiles\Simplified Bridge Solutions\BRIDGframe, or location program is saved in.

If the diagram section of the wall is not visible on the Geometry tab it may be because i) preceding tabs are not synchronized, ii) move cursor over tab to regenerate.

9.0 Limitations

Cross sectional dimensions are constant over length of wall being analyzed.

Forces at bearing seat for abutment design are assumed to act along the centre line of the transverse length of the structure.

Earth fill beyond the length of abutment wall is not included in the abutment analysis.

For pile foundation design, a tool has been provided for axial structural design only. A later version will allow for moment and shear design also.

Longitudinal force at the abutment bearing seat acting against the restrained soil is not available.

Vertical forces causing uplift in the abutment is not available.

APPENDIX 1 - PROGRAM FEATURES

BRIDGwall

Abutment, retainingwall, and gravity wall design software

- conformance with CHBDC and AASHTO
- simple and minimal tabular input
- automatic importing of data from earlier BRIDGwall Excel files
- SLS / Service and ULS / Strength analysis and design
- load combinations pre-set to cover any governing condition
- 'Optimize' options provided to quickly establish minimum footing component widths to satisfy all conditions
- reinforcing steel and pile foundation tool included
- print tab makes printing worksheets simple
- print results are as per they appear on the worksheets
- output is very clearly defined
- output is in Microsoft Excel
- metric or imperial input and results

APPENDIX 2 - SOFTWARE LICENSING AGREEMENT AND INSTALLATION

BRIDGwall Software Licensing Agreement

By installing the BRIDGwall Software (which consists of software, documentation and other items; hereafter: "Software") created by Simplified Bridge Solutions Ltd., you agree to be bound by the terms and conditions of this License Agreement. As used in this License Agreement, "You" shall mean the individual using or installing the Software together with any individual or entity, including but not limited to your employer, on whose behalf you are acting in using or installing the Software. You shall be the "licensee" under this License Agreement.

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4. Support, Upgrades and Service Releases

Simplified Bridge Solutions Ltd. shall offer free technical support that does not fall under the scope of providing engineering services, and product upgrades for the licensed term after purchasing the product. The product license expires at the term end; therefore, you must pay the annual maintenance fee in order to receive a renewal license and ongoing support and product upgrades.

5. Termination

This Agreement is effective until terminated. This Agreement will terminate automatically without notice from Simplified Bridge Solutions Ltd. if you fail to comply with any provision contained herein or if the funds paid for the license are refunded or are not received. Upon termination, you must destroy the Software, and all copies of the Software, in part and in whole, including modified copies if any.

6. Non-Waiver

The failure by either party at any time to enforce any of the provisions of this License Agreement or any right or remedy available hereunder or at law or in equity, or to exercise any option herein provided, shall not constitute a waiver of such provision, right, remedy, or option or in any way affect the validity of this License Agreement. The waiver of any default by either party shall not be deemed a continuing waiver, but shall apply solely to the instance to which such waiver is directed.

BRIDGwall Installation

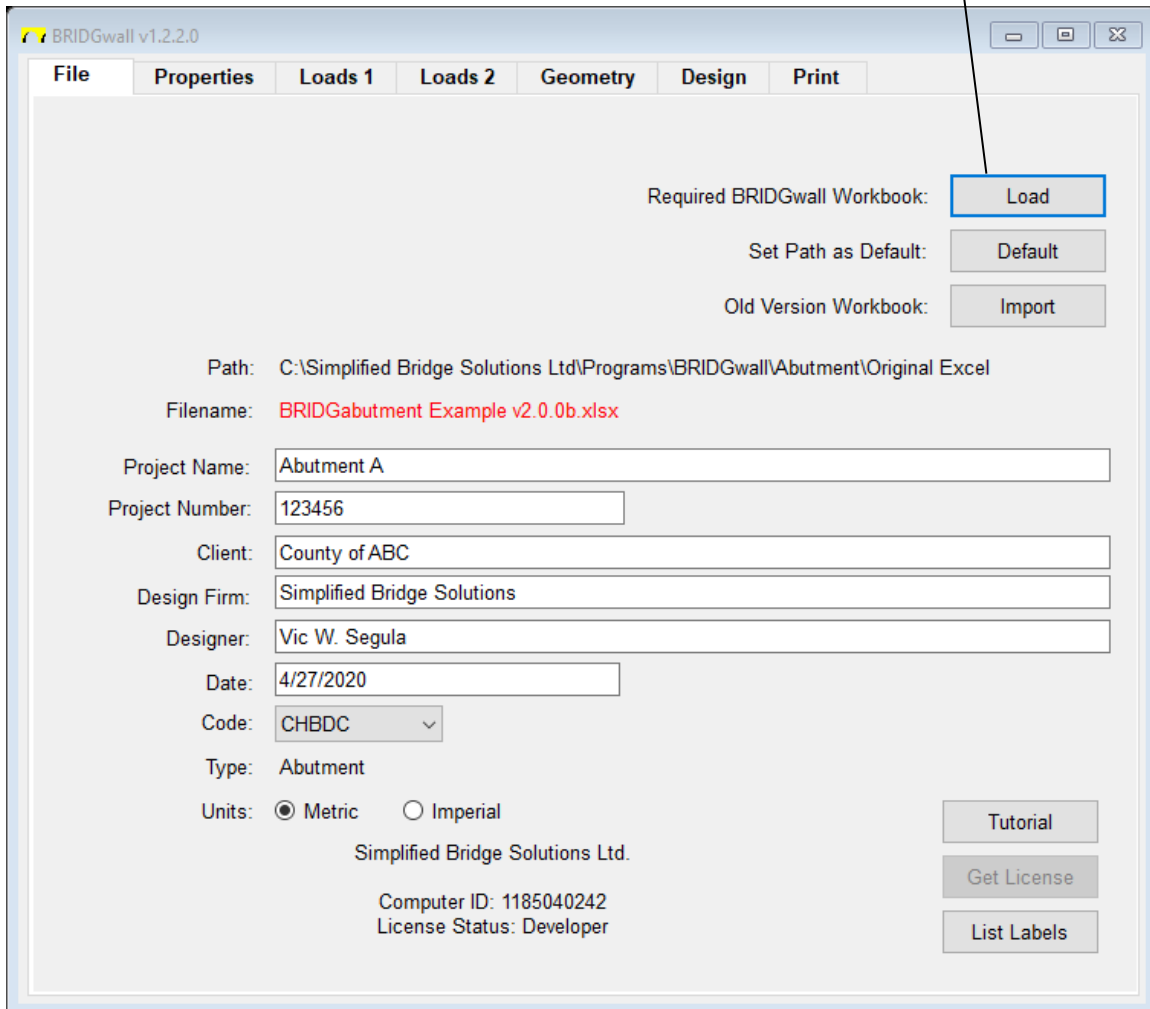
Design parameters and calculation results for retaining soil walls are stored in Excel workbooks, one workbook per design. BRIDGwall is a dialog that provides the User Interface to these Excel workbooks. An example workbook is required as the starting point for your first new analysis. Later analysis may utilize this workbook or other saved workbooks generated from the original Excel file. All files are available for download directly from our website.

Certain advanced features are disabled until the application is registered.

BRIDGwall will run in Demo mode until it is registered.

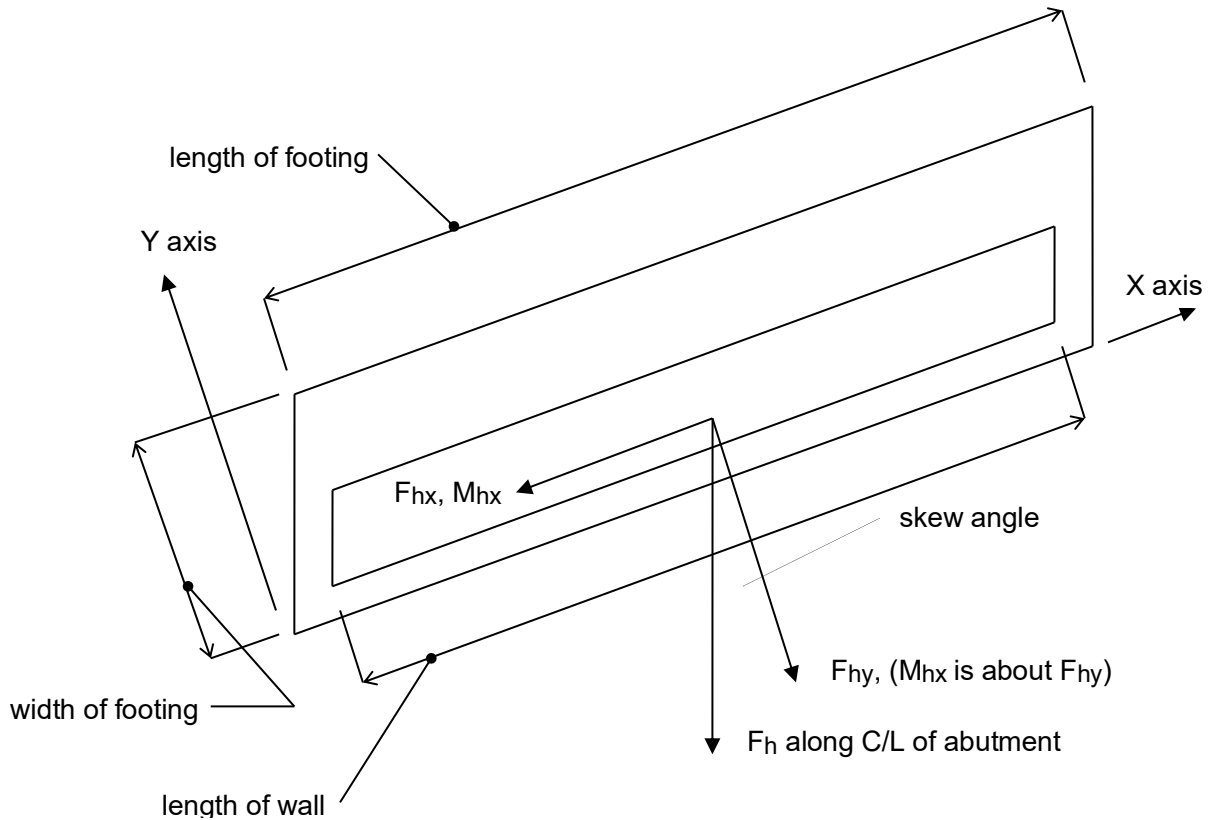
APPENDIX 3 – FILE TAB

BRIDGretainingwall or BRIDGabutment Load button



- Load: load the BRIDGwall Excel file to be used in design
- Default: resets to the path of the loaded excel file, where the program will automatically open to upon reopening
- Import: imports data from one Excel file into the loaded Excel file.
- Input project particulars
- Tutorial: this button provides a link to the web site
- Get License: this button provides a link to the web site

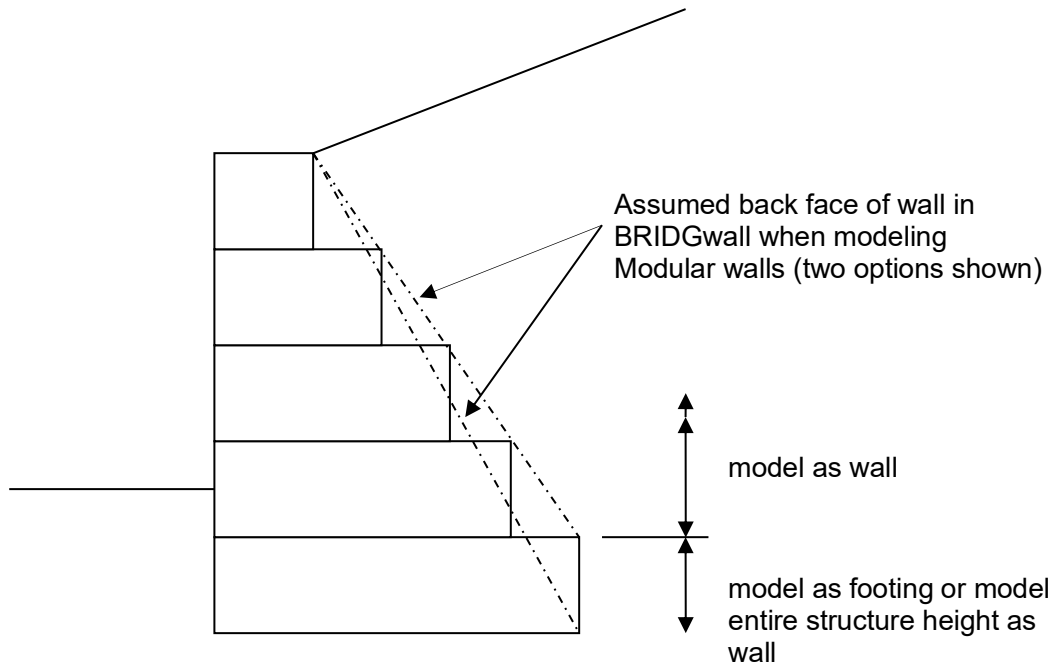
APPENDIX 4 – PLAN GEOMETRY AND APPLICATION OF FORCES



Plan – Abutment

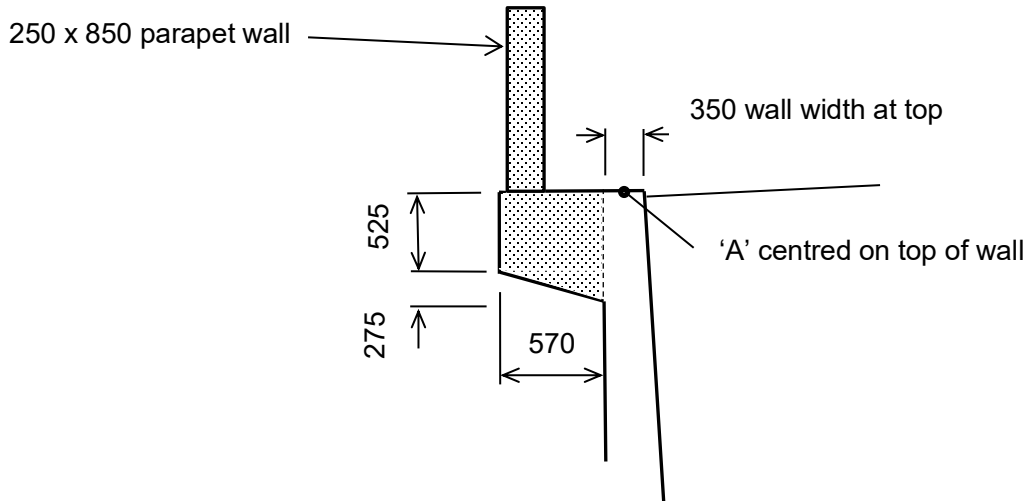
- 'Additional Loads' for abutments as found on the Loads 1 tab provides for load input from the superstructure. Horizontal loads from BRIDGframe due to temperature contraction, shrinkage, etc., may be entered as F_h . BRIDGwall will convert the load to F_{hx} and F_{hy} components.
- Input the total F_h forces. These forces are assumed to act along the centre line of abutment.
- M_{hx} moments are acting about the F_{hy} axis or in the F_{hx} direction
- Although the ends of the footing may be skewed, for simplicity, non-skewed ends are assumed.

APPENDIX 5 – MODULAR WALLS



- When modeling modular walls in BRIDGwall, the gravity wall will form that of a trapezoid
- Refer to Figure 3.11.5.9-2 of AASHTO

APPENDIX 6 – RETAINING WALL



Parapet wall: $0.25 \times 0.85 \times 24 \text{ kN/m}^3 = 5.1 \text{ kN @ } 0.57 \text{ m from A}$

Corbel: rect: $0.525 \times 0.57 \times 24 \text{ kN/m}^3 = 7.2 \text{ kN @ } 0.46 \text{ m from A}$
 tri: $0.275 \times 0.57/2 \times 24 \text{ kN/m}^3 = 1.9 \text{ kN @ } 0.365 \text{ m from A}$

For minimum vertical load, parapet wall weight will be excluded.

$F_v = 14.2 \text{ kN max unfactored}$
 $F_v = 9.1 \text{ kN min unfactored}$

$x = (5.1 \times 0.57 + 7.2 \times 0.46 + 1.9 \times 0.365) / 14.2 = 0.487 \text{ m max}$
 $x = (7.2 \times 0.46 + 1.9 \times 0.365) / 9.1 = 0.440 \text{ m min}$

SLS $F_v \text{ max} = 14.2 \text{ kN}$
 SLS $M_v \text{ max} = 14.2 \times 0.487 = 6.92 \text{ kN.m}$ (positive for rotation away from retained fill)

SLS $F_v \text{ min} = 9.1 \text{ kN}$
 SLS $M_v \text{ min} = 9.1 \times 0.440 = 4.00 \text{ kN.m}$

ULS $F_v \text{ max} = 14.2 \times 1.2 = 17.1 \text{ kN}$
 ULS $M_v \text{ max} = 6.92 \times 1.2 = 8.31 \text{ kN.m}$

ULS $F_v \text{ min} = 9.1 \times 0.9 = 8.2 \text{ kN}$
 ULS $M_v \text{ min} = 4.00 \times 0.9 = 3.60 \text{ kN.m}$

Input above values into Loads 1, Additional Loads, Vertical:

APPENDIX 7 – RETAINING WALL

Backfill slope: 26.6 ° (2 horizontal to 1 vertical)

Effective overburden pressure at toe = resisting backfill density x depth of fill = 1.2 x 16 = 19.2 kPa.

Load factors for EH Righting may be entered as 0 (zero) to eliminate any horizontal resisting earth pressure. Or these same factors may be increased to change horizontal resisting earth pressure from at-rest to passive conditions.

Note: A value greater than zero shall be entered for the Heel Width of Cantilevered Walls when using the Optimize option.

BRIDGwall v2.0.0.10

File Properties Loads 1 Loads 2 Loads 3 Geometry Design Print

Backfill Properties

| | | | |
|--|-----------------------------------|---|-----------------------------------|
| Retained Backfill: | | Resisting Backfill: | |
| Backfill Density (kN/m ³): | <input type="text" value="22"/> | Backfill Density (kN/m ³): | <input type="text" value="16"/> |
| Saturated Backfill Density (kN/m ³): | <input type="text" value="22"/> | Resisting Backfill Height (m): | <input type="text" value="1.5"/> |
| Angle of Wall Friction (degrees): | <input type="text" value="0"/> | Effective Friction Angle (degrees): | <input type="text" value="30"/> |
| Effective Friction Angle (degrees): | <input type="text" value="30"/> | Bearing Material - ULS / Strength: | |
| Wall Rotation (degrees): | <input type="text" value="0"/> | Allowable Concentric Bearing Capacity (kPa): | <input type="text" value="550"/> |
| Height of Water Table (m): | <input type="text" value="1.5"/> | Effective Friction Angle of founding ground (degrees): | <input type="text" value="30"/> |
| Slope of Backfill (degrees): | <input type="text" value="26.6"/> | Effective Friction Angle at u/s of Footing (degrees): | <input type="text" value="30"/> |
| Bearing Material - SLS / Service: | | Effective Cohesion within founding ground (kPa): | <input type="text" value="0"/> |
| Allowable Bearing Capacity (kPa): | <input type="text" value="450"/> | Effective Cohesion at u/s of footing (kPa): | <input type="text" value="0"/> |
| | | Undrained Shear Strength (kPa): | <input type="text" value="0"/> |
| | | Effective Overburden Pressure - toe founding level (kPa): | <input type="text" value="19.2"/> |
| | | Density of Founding Material (kN/m ³): | <input type="text" value="19"/> |

[Click to Update BRIDGretainingwall Example v2.0.23.xlsx](#)

BRIDGwall v2.0.0.10

File Properties **Loads 1** Loads 2 Loads 3 Geometry Design Print

General Loads

Live UDL Surcharge (SLS) (kPa): Permanent UDL Surcharge (SLS) (kPa):

Lateral Seismic Earth Pressure: (ULS) (kPa)

Structure Density (kN/m³):

Additional Loads

Horizontal: SLS Design: ULS Design:

Max. Fh (kN/m): Max. Fh (kN/m):

Min. Fh (kN/m): Min. Fh (kN/m):

Vertical distance from u/s of footing to Fh (m):

Vertical: SLS Design: ULS Design:

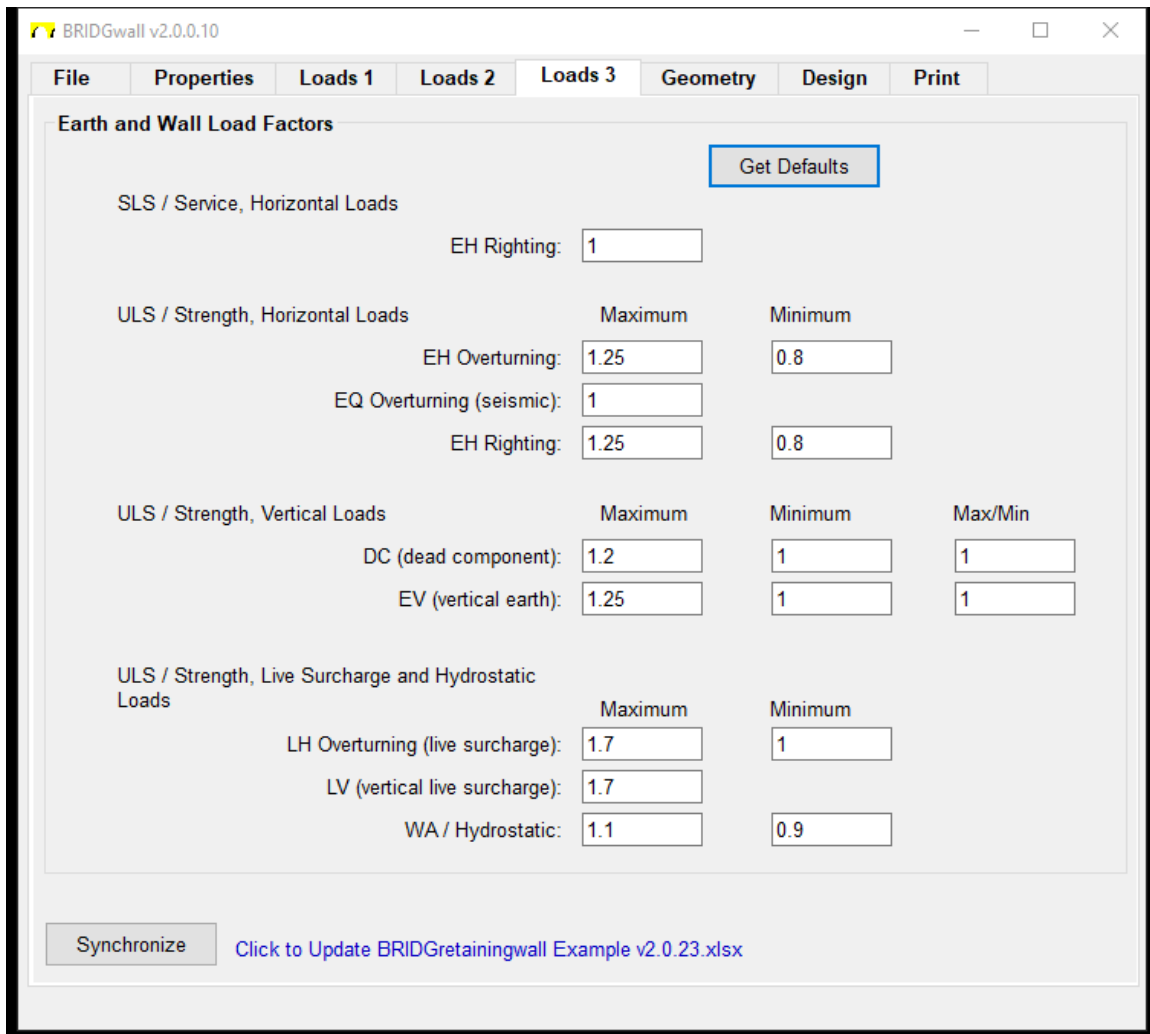
Max. Fv (kN/m): Max. Fv (kN/m):

Corresponding Mv (kN.m/m): Corresponding Mv (kN.m/m):

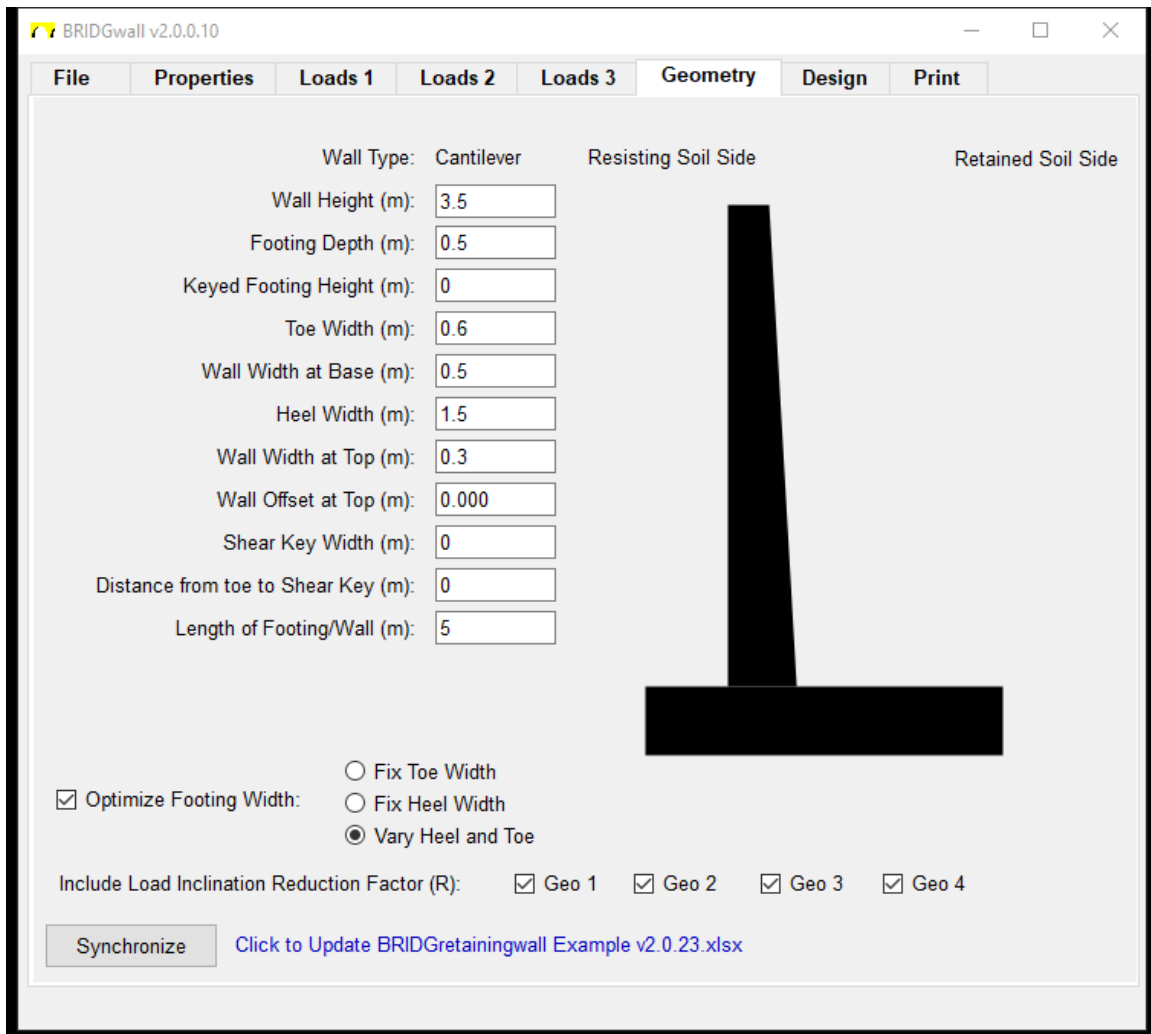
Min. Fv (kN/m): Min. Fv (kN/m):

Corresponding Mv (kN.m/m): Corresponding Mv (kN.m/m):

Synchronize [Click to Update BRIDGretainingwall Example v2.0.23.xlsx](#)



Note: For the two values of LH on the Loads 3 tab, the default value has been set to 1.7 as per C6.12.5. However, MTO is still using 1.25 for these values so the User may decide to overwrite the default values.



APPENDIX 8 – GRAVITY WALL

Angle of Wall Friction: 20° (Note: Entering a value for angle of wall friction determines a gravity wall type. Absence of this value determines a cantilever wall type)

The 'Optimize' button on the Geometry tab will find the smallest toe width. For gravity walls with no toe, do not use the Optimize button.

Effective overburden pressure at toe = resisting backfill density x depth of fill = $1.2 \times 16 = 19.2$ kPa.

Load factors for EH Righting may be entered as 0 (zero) to eliminate any horizontal resisting earth pressure. Or these same factors may be increased to change horizontal resisting earth pressure from at-rest to passive conditions.

Live UDL Surcharge = 2 kPa for snow load

Structure is concrete. For modular walls constructed of gabions or other, use appropriate structure density (Loads 1).

Note: For Gravity Walls with no footings, use a very small footing depth such as 0.0001 m to remove the warning note on the Geometry tab.

BRIDGwall v2.0.0.10

File Properties Loads 1 Loads 2 Loads 3 Geometry Design Print

Backfill Properties

Retained Backfill:

Backfill Density (kN/m³): 22

Saturated Backfill Density (kN/m³): 0

Angle of Wall Friction (degrees): 15

Effective Friction Angle (degrees): 30

Wall Rotation (degrees): 0

Height of Water Table (m): 0

Slope of Backfill (degrees): 0

Resisting Backfill:

Backfill Density (kN/m³): 16

Resisting Backfill Height (m): 1.5

Effective Friction Angle (degrees): 30

Bearing Material - ULS / Strength:

Allowable Concentric Bearing Capacity (kPa): 300

Bearing Material - SLS / Service:

Allowable Bearing Capacity (kPa): 250

Effective Friction Angle of founding ground (degrees): 30

Effective Friction Angle at u/s of Footing (degrees): 30

Effective Cohesion within founding ground (kPa): 0

Effective Cohesion at u/s of footing (kPa): 0

Undrained Shear Strength (kPa): 0

Effective Overburden Pressure - toe founding level (kPa): 19.2

Density of Founding Material (kN/m³): 19

Synchronize Click to Update BRIDGretainingwall Example v2.0.23.xlsx

- Angle of Wall Friction is typically 1/2 to 2/3 of Effective Friction Angle

BRIDGwall v2.0.0.10

File Properties **Loads 1** Loads 2 Loads 3 Geometry Design Print

General Loads

Live UDL Surcharge (SLS) (kPa): Permanent UDL Surcharge (SLS) (kPa):

Lateral Seismic Earth Pressure: (ULS) (kPa)

Structure Density (kN/m³):

Additional Loads

Horizontal:

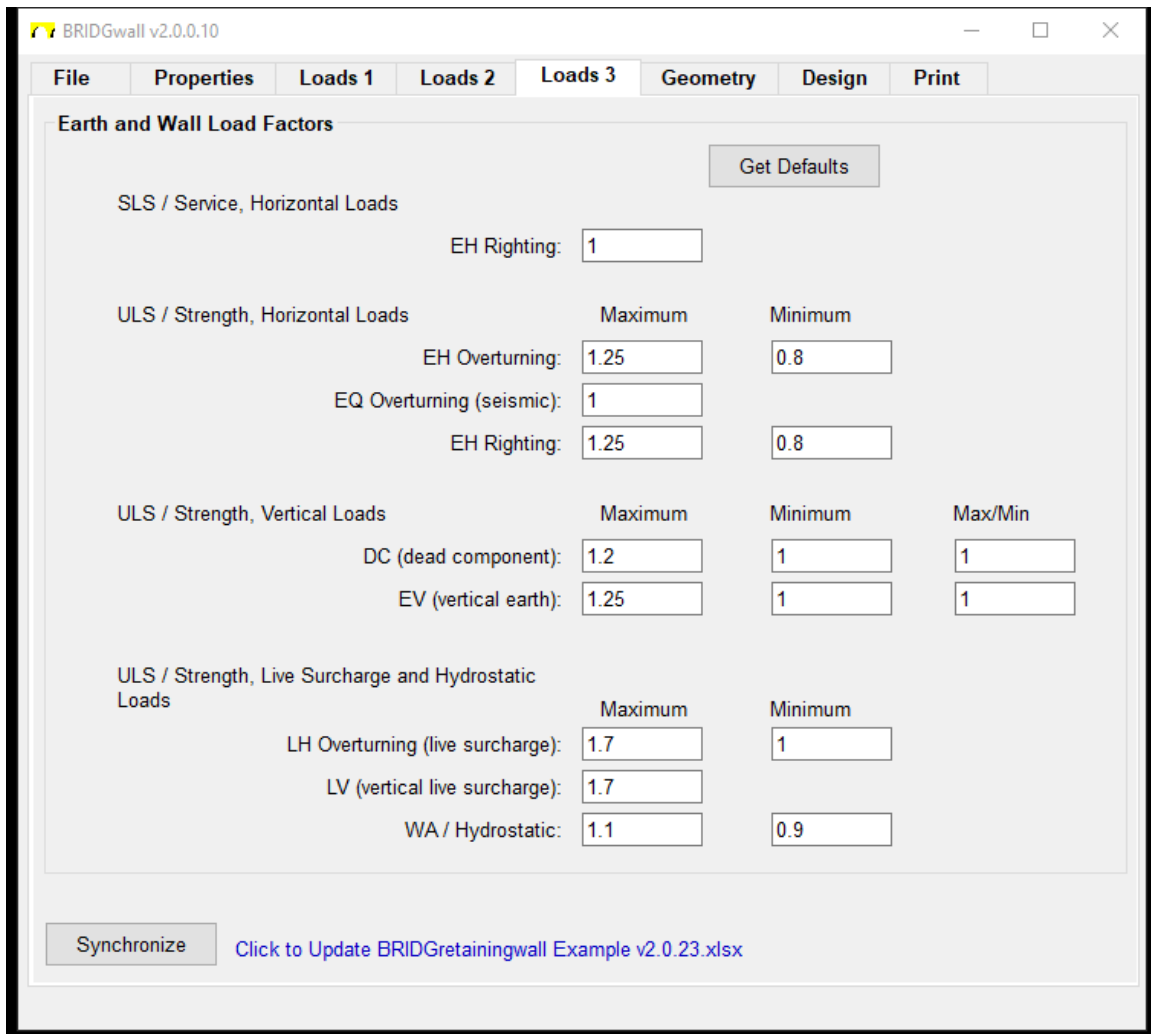
| | | |
|-----------------|--------------------------------|--|
| | SLS Design: | ULS Design: |
| Max. Fh (kN/m): | <input type="text" value="0"/> | Max. Fh (kN/m): <input type="text" value="0"/> |
| Min. Fh (kN/m): | <input type="text" value="0"/> | Min. Fh (kN/m): <input type="text" value="0"/> |

Vertical distance from u/s of footing to Fh (m):

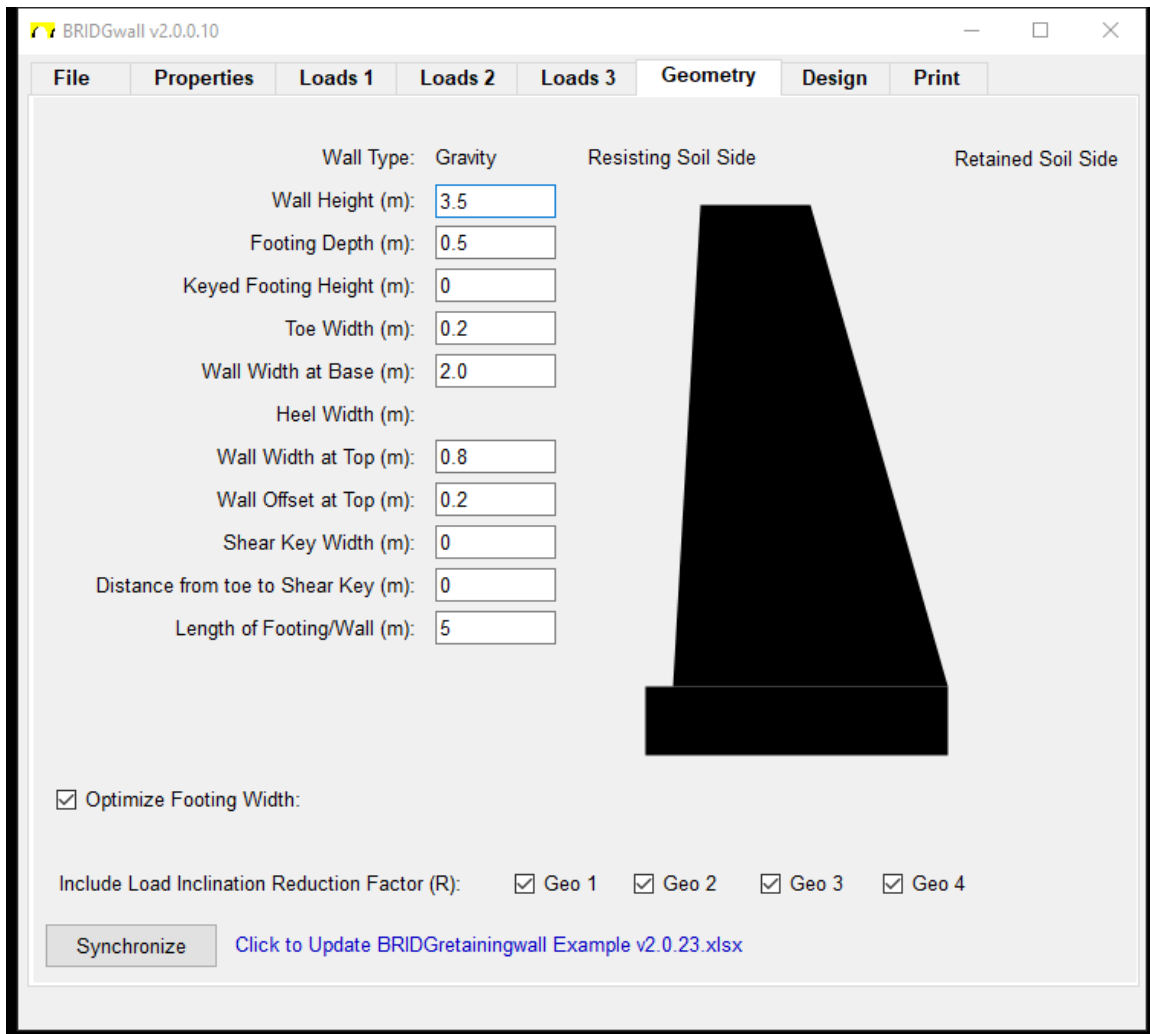
Vertical:

| | | |
|----------------------------|--------------------------------|---|
| | SLS Design: | ULS Design: |
| Max. Fv (kN/m): | <input type="text" value="0"/> | Max. Fv (kN/m): <input type="text" value="0"/> |
| Corresponding Mv (kN.m/m): | <input type="text" value="0"/> | Corresponding Mv (kN.m/m): <input type="text" value="0"/> |
| Min. Fv (kN/m): | <input type="text" value="0"/> | Min. Fv (kN/m): <input type="text" value="0"/> |
| Corresponding Mv (kN.m/m): | <input type="text" value="0"/> | Corresponding Mv (kN.m/m): <input type="text" value="0"/> |

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Note: For the two values of LH on the Loads 3 tab, the default value has been set to 1.7 as per C6.12.5. However, MTO is still using 1.25 for these values so the User may decide to overwrite the default values.



APPENDIX 9 – DEEP PILE FOUNDATION TO CHBDC

Abutment Geometry

Bridge structure data: 13 girders / span semi-continuous with semi-integral abutments

Abutment data: (Distance between top of road and top of abutment \cong 650 mm)

Skew: 30 °
Wall length: 29.951 m perpendicular to road, therefore skewed length = 34.585 m
Footing length: say same as skewed wall length = 34.585 m
Wall dimensions: see input sheet screen prints
Piles: HS 324 dia.
ULS geotechnical compressive resistance = 620 kN
tension resistance = 600 kN
SLS geotechnical compressive resistance = 415 kN
tension resistance = 400 kN
Initially assuming SLS and ULS horizontal resistance of piles is not required

Step 1) Produce a model assuming no piles. (From results the applicable forces will be used for pile design)

Total loading at bearing seat (from BRIDGframe) at SLS and showing ULS 3:

Note: The following example is for ULS 3; other ULS are also applicable, including during construction conditions. Using vertical loads from wingwalls only; ignoring moments.

SLS Vertical:

Transitory loads: 1697 kN
Remaining loads: 4120 kN (incl. weight of wingwalls / barriers on wingwalls)

ULS 3 Vertical:

Max. transitory loads: 2713 kN
Min. transitory loads: -679 kN
Max. remaining loads: 4497 kN (incl. weight of wingwalls / barriers on wingwalls)
Min. remaining loads: 3181 kN (incl. weight of wingwalls / barriers on wingwalls)

SLS Horizontal: (ignoring eccentricity of wingwalls / barriers on wingwalls)

Temperature Contraction: load factor = 0.8

13 bearings with horizontal shear stiffness of 4.0 kN / mm / brg
Contraction movement = 16.7

Max. corresponding load: $13 \times 4.0 \times 16.7 \times 0.8 = 695 \text{ kN}$

ULS 3 Horizontal (Longitudinal): (ignoring eccentricity of wingwalls / barriers on wingwalls)

Temperature Contraction: load factor = 1.0

Max. corresponding load: $13 \times 4.0 \times 16.7 \times 1.0 = 868 \text{ kN}$
Min. corresponding load: say = 0 kN (would be negative for expansion)

SLS Horizontal (Transverse): Transitory

Transverse Wind Load on Superstructure: N/A
Transverse Wind Load on Live Load: N/A

Transverse Temperature Contraction:
(transverse loading from temperature will be automatically calculated by program)

ULS 3 Horizontal (Transverse): Transitory

Transverse Wind Load on Superstructure: acting 1.38 m above the bearing seat

$F_{hx} = 24 \times 0.45 = 11 \text{ kN}$
 $M_{hx} = 11 \times (1.38 + \text{abut wall ht} + \text{ftg dpth})$
 $= 11 \times (1.38 + 1.7 + 0.7) = 42 \text{ kN.m}$

Transverse Wind Load on Live Load: acting 3.74 m above the bearing seat

$F_{hx} = 24 \times 0.45 = 11 \text{ kN}$
 $M_{hx} = 11 \times (3.74 + 1.7 + 0.7) = 68 \text{ kN.m}$

Transverse Temperature Contraction:
(transverse loading from temperature will be automatically calculated by program)

Surcharge Loads:

Backfill: $0.65 \times 21.2 = 13.78 \text{ kPa}$ (top of abutment is 0.65 m below grade)
Live: $0.8 \times 21.2 = 16.96 \text{ kPa}$. If the bridge consists of 8 lanes, use 3.0m wide per lane. Therefore, use a Live of $16.96 \times 8 \times 3 / 34.585 = 11.77 \text{ kPa}$

Effective overburden pressure at toe = resisting backfill density x depth of fill = $1.2 \times 16 = 19.2 \text{ kPa}$.

Assume SLS and ULS allowable bearing capacities as a starting point only for approximating footing size; they are not applicable to the pile foundation design.

Load factors for EH Righting may be entered as 0 (zero) to eliminate any horizontal resisting earth pressure. Or these same factors may be increased to change horizontal resisting earth pressure from at-rest to passive conditions.

BRIDGwall v2.0.0.10

File Properties Loads 1 Loads 2 Loads 3 Geometry Design Print

Backfill Properties

| | | | |
|--|----------------------------------|---|-----------------------------------|
| Retained Backfill: | | Resisting Backfill: | |
| Backfill Density (kN/m ³): | <input type="text" value="22"/> | Backfill Density (kN/m ³): | <input type="text" value="16"/> |
| Angle of Wall Friction (degrees): | <input type="text" value="0"/> | Resisting Backfill Height (m): | <input type="text" value="1.2"/> |
| Effective Friction Angle (degrees): | <input type="text" value="30"/> | Effective Friction Angle (degrees): | <input type="text" value="30"/> |
| Road Top to Abutment Top (m): | <input type="text" value="0.7"/> | Bearing Material - ULS / Strength: | |
| | | Allowable Concentric Bearing Capacity (kPa): | <input type="text" value="500"/> |
| | | Effective Friction Angle of founding ground (degrees): | <input type="text" value="30"/> |
| Bearing Material - SLS / Service: | | Effective Friction Angle at u/s of Footing (degrees): | <input type="text" value="30"/> |
| Allowable Bearing Capacity (kPa): | <input type="text" value="450"/> | Effective Cohesion within founding ground (kPa): | <input type="text" value="0"/> |
| | | Effective Cohesion at u/s of footing (kPa): | <input type="text" value="0"/> |
| | | Undrained Shear Strength (kPa): | <input type="text" value="0"/> |
| | | Effective Overburden Pressure - toe founding level (kPa): | <input type="text" value="19.2"/> |
| | | Density of Founding Material (kN/m ³): | <input type="text" value="20"/> |

[Click to Update BRIDGabutment Example v2.0.23.xlsx](#)

BRIDGwall v2.0.0.12

File Properties **Loads 1** Loads 2 Loads 3 Geometry Design Print

General Loads

Live UDL Surcharge (SLS) (kPa): Permanent UDL Surcharge (SLS) (kPa):

Lateral Seismic Earth Pressure: (ULS) (kPa)

Use Approach Slabs: Structure Density (kN/m³):

Additional Vertical Loads

| In Y Direction: | SLS Design: | ULS Design: |
|--|--|--|
| Max. Fv (kN): <input type="text" value="0"/> | Max. Fv (kN): <input type="text" value="0"/> | Max. Fv (kN): <input type="text" value="0"/> |
| Corres. Righting Moment (kN.m): <input type="text" value="0"/> | Corres. Righting Moment (kN.m): <input type="text" value="0"/> | Corres. Righting Moment (kN.m): <input type="text" value="0"/> |
| Min. Fv (kN): <input type="text" value="0"/> | Min. Fv (kN): <input type="text" value="0"/> | Min. Fv (kN): <input type="text" value="0"/> |
| Corres. Righting Moment (kN.m): <input type="text" value="0"/> | Corres. Righting Moment (kN.m): <input type="text" value="0"/> | Corres. Righting Moment (kN.m): <input type="text" value="0"/> |

Fv is applied to create a uniform soil bearing pressure over footing plan. Righting Moment is about point X of footing

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- Vertical Additional Loads may be used to model the portion of wingalls that extend beyond the heel of the footing. The portion of the wingwall that is directly over the heel of the footing will be modeled as backfill by the program, and since concrete and backfill are approximately the same weight, the portion of wingwall over the heel is being accounted for.
- If the Heel Width is calculated by the program, the actual forces from the wingwall may need to be recalculated for consistency.

BRIDGwall v2.0.0.10

File Properties Loads 1 Loads 2 Loads 3 Geometry Design Print

Loads on Bearing Seat

| | SLS Design: | ULS Design: |
|--------------------------------|--------------------------------|-----------------------------------|
| Max. Fv transitory loads (kN): | <input type="text" value="0"/> | <input type="text" value="2713"/> |
| Max. Fv remaining loads (kN): | <input type="text" value="0"/> | <input type="text" value="4497"/> |
| Min. Fv transitory loads (kN): | <input type="text" value="0"/> | <input type="text" value="-697"/> |
| Min. Fv remaining loads (kN): | <input type="text" value="0"/> | <input type="text" value="3181"/> |
| Corresponding Max. Fh (kN): | <input type="text" value="0"/> | <input type="text" value="868"/> |
| Corresponding Min. Fh (kN): | <input type="text" value="0"/> | <input type="text" value="0"/> |

Transverse Load (excluding Fhx from Fh)

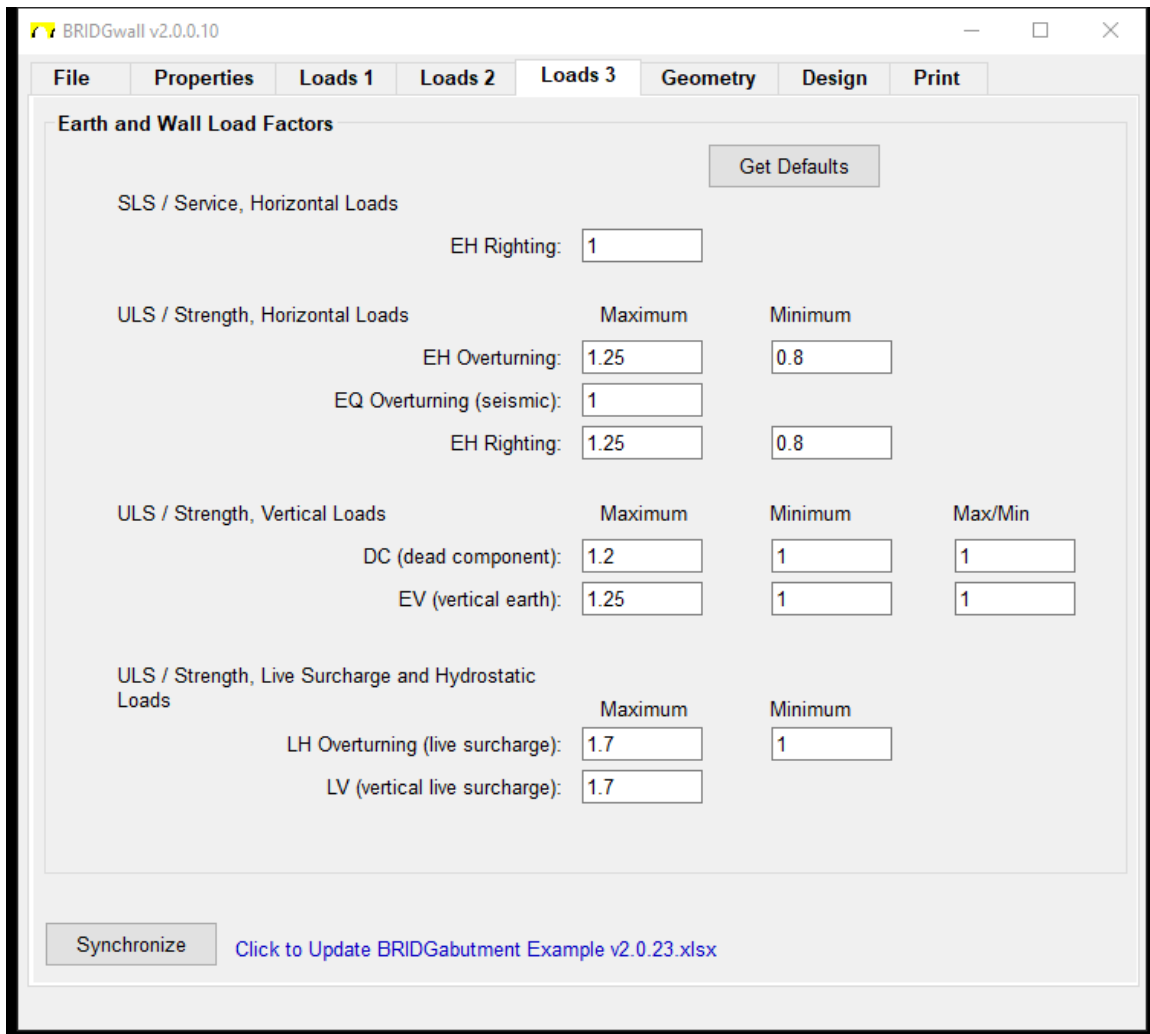
| | SLS Design: | ULS Design: |
|---|--------------------------------|----------------------------------|
| Additional Fhx (kN): | <input type="text" value="0"/> | <input type="text" value="22"/> |
| Mhx from Max. Fv transitory loads (kN.m): | <input type="text" value="0"/> | <input type="text" value="110"/> |
| Mhx from Max. Fv remaining loads (kN.m): | <input type="text" value="0"/> | <input type="text" value="0"/> |
| Mhx from Min. Fv transitory loads (kN.m): | <input type="text" value="0"/> | <input type="text" value="90"/> |
| Mhx from Min. Fv remaining loads (kN.m): | <input type="text" value="0"/> | <input type="text" value="0"/> |

Fh and Fhx is applied at bearing seat
Mhx using vert. loads is eccentric loads from mid-length of footing

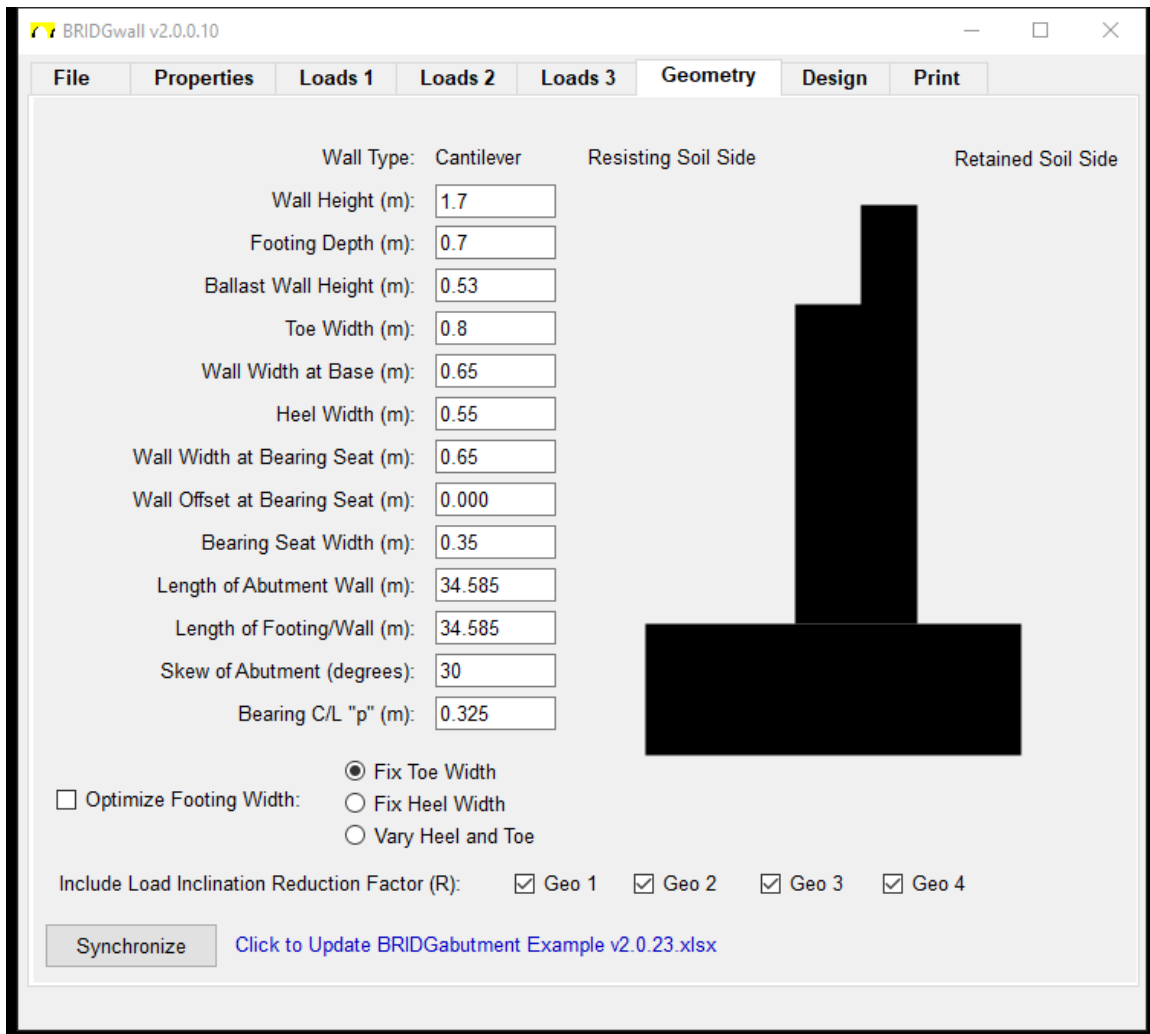
Synchronize [Click to Update BRIDGabutment Example v2.0.23.xlsx](#)

Example:

- Corresponding Max Fh might be if Max Fv transitory included live load, then Max Fh could include braking. If Fv did not include truck load then Fy would not include braking.
- Corresponding Fh may be for temperature only where no value for temperature might be in Fv.
- Corresponding Min Fh will likely always be 0



Note: For the two values of LH on the Loads 3 tab, the default value has been set to 1.7 as per C6.12.5. However, MTO is still using 1.25 for these values so the User may decide to overwrite the default values.



- For simplicity, enter length of abutment and length of footing as the same value. Additional soil fill on the footing that extends past the abutment wall length is not included in design. The length of the footing is only used for calculating bearing resistance as per cl.6.10.2 (CHBDC)

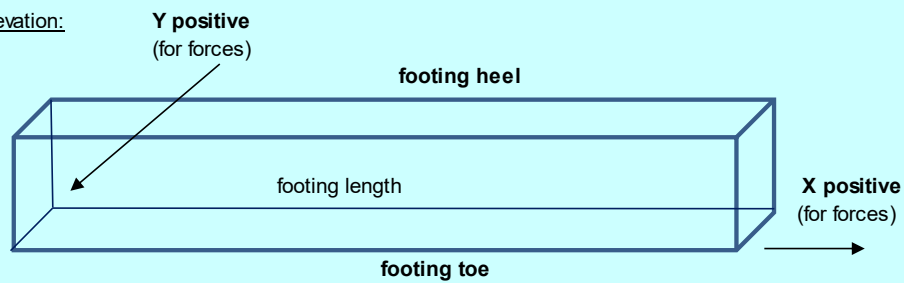
Project Name: Bridge ABC
 Project Number: 123456
 Client: County of ABC
 Design Firm: Simplified Bridge Solutions Ltd.
 Designer: Vic W. Segula
 Date: 14-Jan-24
 Version: 2.0.23
 Type: Abutment
 Code: CHBDC

ABUTMENT WALL DESIGN TO THE CANADIAN HIGHWAY BRIDGE DESIGN CODE

*

Notes: 1) assumes free draining granular backfill and drains, therefore no water or negligible water table cl.C6.9.1(h)

Footing Elevation:

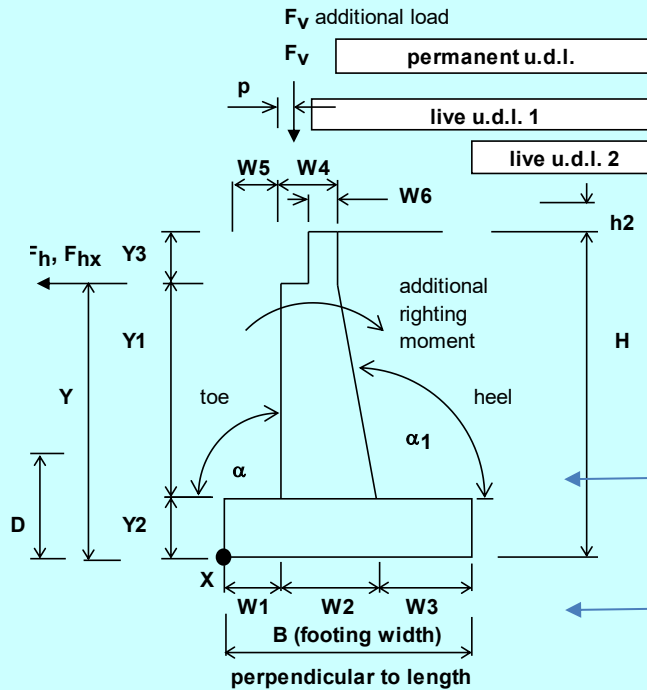


Properties:

| | | |
|------|-------|---|
| Y1 = | 1.700 | m |
| Y2 = | 0.700 | m |
| Y3 = | 0.530 | m |
| W1 = | 0.800 | m |
| W2 = | 0.650 | m |
| W3 = | 0.550 | m |
| W4 = | 0.650 | m |
| W5 = | 0.800 | m |
| W6 = | 0.300 | m |
| p = | 0.325 | m |

Design for: **Cantilever** Wall

| | | |
|-----|-------|---|
| Y = | 2.400 | m |
| B = | 2.000 | m |
| H = | 2.930 | m |



Inclined wall angle from horiz. " α " = 90.0 °
 Inclined wall angle from horiz. " α_1 " = 90.0 °

Length of abutment wall "L1" = 34.585 m
 Length of footing "L2" = 34.585 m
 Skew of abutment = 30.0 °

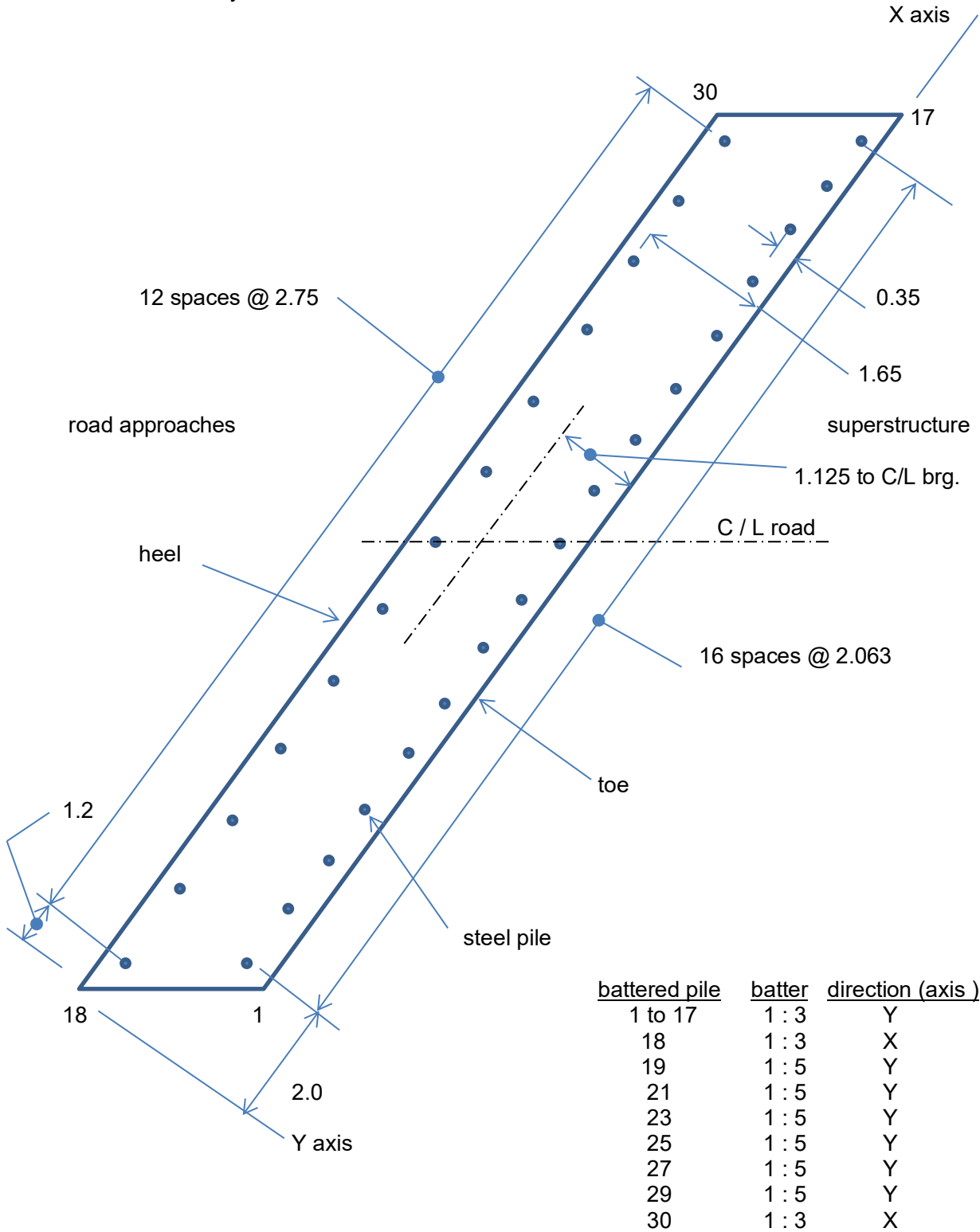
Note: abutment wall is assumed to be centred along length of footing

Structure density = 24.0 kN/m³

Forces on Bearing Seats at 'p' :

| | | | |
|------|---|--------|------|
| SLS: | Max. Fv transitory load (excl. DLA) = | 0.0 | kN |
| | Max. Fv remaining loads = | 0.0 | kN |
| | Min. Fv transitory load (excl. DLA) = | 0.0 | kN |
| | Min. Fv remaining loads = | 0.0 | kN |
| | Max. Fh force = | 0.0 | kN |
| | Min. Fh force = | 0.0 | kN |
| | Corresp. Max. Fhy force (from Fh) = | 0.0 | kN |
| | Corresp. Max. Fhx force (from Fh) = | 0.0 | kN |
| | Corresp. Min. Fhy force (from Fh) = | 0.0 | kN |
| | Corresp. Min. Fhx force (from Fh) = | 0.0 | kN |
| | Additional transverse Fhx = | 0.0 | kN |
| | Mhx from additional transverse Fhx = | 0.0 | kN.m |
| | Mhx using Max. Fv transitory loads = | 0.0 | kN.m |
| | Mhx using Max. Fv remaining loads = | 0.0 | kN.m |
| | Mhx using Min. Fv transitory loads = | 0.0 | kN.m |
| | Mhx using Min. Fv remaining loads = | 0.0 | kN.m |
| ULS: | Max. Fv transitory load (excl. DLA) = | 2713.0 | kN |
| | Max. Fv remaining loads = | 4497.0 | kN |
| | Min. Fv transitory load (excl. DLA) = | -697.0 | kN |
| | Min. Fv remaining loads = | 3181.0 | kN |
| | Max. Fh force = | 868.0 | kN |
| | Min. Fh force = | 0.0 | kN |
| | Corresp. Max. Fhy force (from Fh) = | 751.7 | kN |
| | Corresp. Max. Fhx force (from Fh) = | 434.0 | kN |
| | Corresp. Min. Fhy force (from Fh) = | 0.0 | kN |
| | Corresp. Min. Fhx force (from Fh) = | 0.0 | kN |
| | Additional transverse Fhx = | 22.0 | kN |
| | Mhx from additional transverse Max. Fhx = | 52.8 | kN.m |
| | Mhx using Max. Fv transitory loads = | 110.0 | kN.m |
| | Mhx using Max. Fv remaining loads = | 0.0 | kN.m |
| | Mhx using Min. Fv transitory loads = | 90.0 | kN.m |
| | Mhx using Min. Fv remaining loads = | 0.0 | kN.m |

Assumed Pile Layout:



Conservatively assume unsupported length of pile = 6000 mm.

| Resisting Soil: | | min. horizontal earth | | |
|---|----------|------------------------------|-----|---|
| SLS: | | | | |
| $P_{Ohy} = K_o (0.5 \times \text{density soil} \times H^2) \times L1 =$ | | 199.2 | kN | |
| ULS: | | | | |
| $P_{Ohy} = K_o (0.5 \times \text{density soil} \times H^2) \times L1 =$ | | 159.4 | kN | |
| Vertical distance from X to $P_{Ohy} =$ | | 0.400 | m | |
| <u>CANTILEVER WALL</u> * | | | | |
| Sum of Horizontal Forces " P_{Hy} " = | 1477.0 | kN | SLS | |
| Sum of Horizontal Forces " P_{Hy} " = | 2687.6 | kN | ULS | ← |
| Sum of Horizontal Forces " P_{Hx} " = | 0.0 | kN | SLS | |
| Sum of Horizontal Forces " P_{Hx} " = | 456.0 | kN | ULS | ← |
| Moment Righting " M_{Ry} " = | 5140.6 | kN.m | SLS | |
| Moment Righting " M_{Ry} " = | 14628.1 | kN.m | ULS | ← |
| Moment Righting " M_{Rx} " = | 68718.7 | kN.m | SLS | |
| Moment Righting " M_{Rx} " = | 211357.9 | kN.m | ULS | ← |
| Moment Overturning " M_{Oy} " = | 2062.1 | kN.m | SLS | |
| Moment Overturning " M_{Oy} " = | 4381.8 | kN.m | ULS | ← |
| Moment about C/L of footing " M_{Ox} " = | 0.0 | kN.m | SLS | |
| Moment about C/L of footing " M_{Ox} " = | 1204.4 | kN.m | ULS | ← |
| Sum of Vertical Loads " V " = | 3973.9 | kN | SLS | |
| Sum of Vertical Loads " Q " = | 12222.5 | kN | ULS | ← |

$Mx1$ = X direction moments about Y axis from Gravity loads.

Note: if the center of the gravity loads about the Y axis passes through the centroid of the piles about the Y axis, the above $Mx1$ is not required. This example will include it regardless.

Therefore, $Mx1 = 12514.4 \text{ kN} \times 17.293 \text{ m} = 216412 \text{ kN.m}$

Torsion:

Torsion is caused by the longitudinal or transverse loads acting at a distance from the centroid of the piles. For transverse force, the location of the force along the Y axis would be the centroid of the bearing.

Distance between centroid of bearing and centroid of piles:

Distance from X axis to centroid of bearing = 1.125 m

From the Design 2 worksheet (after completing pile layout tables, the 'y' for torsional moment of inertia = 1.650 m.

$1.650 - 1.125 = 0.525 \text{ m}$

Say wind is acting in same direction as F_h . Torsion is counterclockwise.

$T_y = 2688.4 \text{ kN} \times 0.0 \text{ m} = 0 \text{ kN.m}$ (resultant force acts through centroid of piles)

$T_x = (434.0 + 22.0) \text{ kN} \times 0.525 = -239.4 \text{ kN.m}$ (counterclockwise)

WORKSHEET FOR DEEP PILE FOUNDATION USING CSA-S6-25

Note: For design of piles, set minimum load factor on the Loads 3 Input tab to 1.0 for Dead / SIDL and Vertical Earth Loads

PILE LAYOUT NOTE: Y axis to pass through C/L of footing

'Y' axis (positive direction reversed for pile design for ease of input)

Abutment Wall

side of footing (relative to skew),

C/L of footing

○ - pile

front face of footing toe and 'X' axis (positive direction)

IN Y DIRECTION (ABOUT X AXIS) enter all batters as positive regardless of direction

| Nº of piles ' y ' | pile I.D. | dist. from X axis (m) | Inertia ' y ' of piles | Y batter Y = 'yes' | battered e.g., 4 | rot. from Y axis | rot. from X axis |
|-------------------|-----------|-----------------------|------------------------|--------------------|------------------|------------------|------------------|
| 1 | 1 | 0.350 | 0.317 | Y | 3.000 | 0.0 | 90.0 |
| 1 | 2 | 0.350 | 0.317 | Y | 3.000 | 0.0 | 90.0 |
| 1 | 3 | 0.350 | 0.317 | Y | 3.000 | 0.0 | 90.0 |
| 1 | 4 | 0.350 | 0.317 | Y | 3.000 | 0.0 | 90.0 |
| 1 | 5 | 0.350 | 0.317 | Y | 3.000 | 0.0 | 90.0 |
| 1 | 6 | 0.350 | 0.317 | Y | 3.000 | 0.0 | 90.0 |
| 1 | 7 | 0.350 | 0.317 | Y | 3.000 | 0.0 | 90.0 |
| 1 | 8 | 0.350 | 0.317 | Y | 3.000 | 0.0 | 90.0 |
| 1 | 9 | 0.350 | 0.317 | Y | 3.000 | 0.0 | 90.0 |
| 1 | 10 | 0.350 | 0.317 | Y | 3.000 | 0.0 | 90.0 |
| 1 | 11 | 0.350 | 0.317 | Y | 3.000 | 0.0 | 90.0 |
| 1 | 12 | 0.350 | 0.317 | Y | 3.000 | 0.0 | 90.0 |
| 1 | 13 | 0.350 | 0.317 | Y | 3.000 | 0.0 | 90.0 |
| 1 | 14 | 0.350 | 0.317 | Y | 3.000 | 0.0 | 90.0 |
| 1 | 15 | 0.350 | 0.317 | Y | 3.000 | 0.0 | 90.0 |
| 1 | 16 | 0.350 | 0.317 | Y | 3.000 | 0.0 | 90.0 |
| 1 | 17 | 0.350 | 0.317 | Y | 3.000 | 0.0 | 90.0 |
| 1 | 18 | 1.650 | 0.543 | | | 90.0 | 0.0 |
| 1 | 19 | 1.650 | 0.543 | Y | 5.000 | 0.0 | 90.0 |
| 1 | 20 | 1.650 | 0.543 | | | 0.0 | 0.0 |
| 1 | 21 | 1.650 | 0.543 | Y | 5.000 | 0.0 | 90.0 |
| 1 | 22 | 1.650 | 0.543 | | | 0.0 | 0.0 |
| 1 | 23 | 1.650 | 0.543 | Y | 5.000 | 0.0 | 90.0 |
| 1 | 24 | 1.650 | 0.543 | | | 0.0 | 0.0 |
| 1 | 25 | 1.650 | 0.543 | Y | 5.000 | 0.0 | 90.0 |
| 1 | 26 | 1.650 | 0.543 | | | 0.0 | 0.0 |
| 1 | 27 | 1.650 | 0.543 | Y | 5.000 | 0.0 | 90.0 |
| 1 | 28 | 1.650 | 0.543 | | | 0.0 | 0.0 |
| 1 | 29 | 1.650 | 0.543 | Y | 5.000 | 0.0 | 90.0 |
| 1 | 30 | 1.650 | 0.543 | | | 90.0 | 0.0 |
| | 31 | | | | | | |
| | 32 | | | | | | |

30 = Total piles Battered Piles = 23

$$y' = \text{Sum piles} * \text{dist. from X axis} / \text{Sum piles} = \quad \quad \quad 0.913 \quad \text{m}$$

$$e_y = \text{dist. from X axis}$$

$$\text{Inertia of a single pile in the Y direction} = 1 * (e_y - y')^2$$

$$\text{Inertia of piles ' y ' in the Y direction} = \quad \quad \quad 12.450 \quad \text{m}^4$$

IN X DIRECTION (ABOUT Y AXIS) enter all batters as positive regardless of direction

| Nº of piles ' x ' | pile I.D. | dist. from Y axis (m) | Inertia ' x ' | X batter Y = 'yes' | battered e.g., 4 | actual batter in 'xy' direction |
|-------------------|-----------|-----------------------|---------------|--------------------|------------------|---------------------------------|
| 1 | 1 | 2.000 | 261.026 | | | |
| 1 | 2 | 4.063 | 198.621 | | | |
| 1 | 3 | 6.126 | 144.728 | | | |
| 1 | 4 | 8.189 | 99.347 | | | |
| 1 | 5 | 10.252 | 62.478 | | | |
| 1 | 6 | 12.315 | 34.121 | | | |
| 1 | 7 | 14.378 | 14.276 | | | |
| 1 | 8 | 16.441 | 2.942 | | | |
| 1 | 9 | 18.504 | 0.121 | | | |
| 1 | 10 | 20.567 | 5.811 | | | |
| 1 | 11 | 22.630 | 20.014 | | | |
| 1 | 12 | 24.693 | 42.728 | | | |
| 1 | 13 | 26.756 | 73.955 | | | |
| 1 | 14 | 28.819 | 113.693 | | | |
| 1 | 15 | 30.882 | 161.943 | | | |
| 1 | 16 | 32.945 | 218.706 | | | |
| 1 | 17 | 35.008 | 283.980 | | | |
| 1 | 18 | 1.200 | 287.516 | Y | 3.000 | |
| 1 | 19 | 3.950 | 201.819 | | | |
| 1 | 20 | 6.701 | 131.224 | | | |
| 1 | 21 | 9.451 | 75.782 | | | |
| 1 | 22 | 12.201 | 35.466 | | | |
| 1 | 23 | 14.951 | 10.274 | | | |
| 1 | 24 | 17.702 | 0.206 | | | |
| 1 | 25 | 20.452 | 5.270 | | | |
| 1 | 26 | 23.202 | 25.459 | | | |
| 1 | 27 | 25.952 | 60.773 | | | |
| 1 | 28 | 28.703 | 111.233 | | | |
| 1 | 29 | 31.453 | 176.802 | | | |
| 1 | 30 | 34.203 | 257.497 | Y | 3.000 | |
| | 31 | | | | | |
| | 32 | | | | | |

30 = Total piles Battered Piles = 2

$$x' = \text{Sum piles} * \text{dist. from Y axis} / \text{Sum piles} = \quad 18.156 \quad \text{m}$$

e_x = dist. from Y axis

$$\text{Inertia of a single pile in the X direction} = 1 * (e_x - x')^2$$

$$\text{Inertia of piles ' x ' in the X direction} = \quad 3117.812 \quad \text{m}^4$$

TORSIONAL MOMENT OF INERTIA

- using battered piles only

Y BATTERED PILES

$$x' = \text{Sum piles} \times \text{dist. X} / \text{Sum piles} = 18.295 \text{ m}$$

e_y = dist. from Y axis

$$\text{Inertia of a single pile in the Y direction} = 1 * (x' - e_y)^2$$

$$\text{Inertia of all piles in the Y direction} = 2268.771 \text{ m}^4$$

X BATTERED PILES

$$y' = \text{Sum piles} \times \text{dist. Y} / \text{Sum piles} = 1.650 \text{ m}$$

e_x = dist. from X axis

$$\text{Inertia of a single pile in the X direction} = 1 * (y' - e_x)^2$$

$$\text{Inertia of all piles in the X direction} = 0.000 \text{ m}^4$$

$$\text{Therefore } J = I_x + I_y = 2268.771 \text{ m}^4$$



The screenshot shows the BRIDGwall v2.0.0.12 software interface. The 'Design' tab is active, displaying two main sections: 'Rebar Design' and 'Pile Foundation Design'.

Rebar Design:

- SLS Design:** Moment (kN.m/m): 0, Axial (kN/m): 0
- ULS Design:** Moment (kN.m/m): 0, Axial (kN/m): 0, Shear (kN/m): 0

Pile Foundation Design:

- Sum of Vertical Loads (kN): 12222.5
- Sum of Horizontal Loads (kN):
 - in Y direction (Hy): -2687.6
 - in X direction (Hx): 456.0
- Righting Moments from Vertical Loads (kN.m): 14628.1
- Overturning Moments from Horizontal Loads (kN.m):
 - in Y direction about X axis: -4381.8
 - in X direction about Y axis: 0
- Additional Moments (kN.m):
 - in X direction about mid-length of footing: 1204.4
- Torsion about Battered Piles Centroid:
 - from Hy:
 - Clockwise (kN.m): 0
 - Counterclockwise (kN.m): 0
 - from Hx:
 - Clockwise (kN.m): 0
 - Counterclockwise (kN.m): -239.4

At the bottom of the form, there is a 'Synchronize' button and a link: 'Click to Update BRIDGabutment Example v2.0.31.xlsx'.

- The sign convention in the Y direction has been reversed from that in the remainder of the program for ease of not inputting numerous pile offsets as negative values. Therefore, force direction in the Y direction has changed accordingly.
- Sign convention of horizontal forces should be entered relative to the direction of skew. For clockwise skew, the forces in the X direction will be positive; and for counterclockwise skew, the forces in the X direction will be negative.

PILE DESIGNLOAD DATA - total loads on pile group

Note: V, H, and M forces must be input using program (VB interface)

V = sum of vertical loads = 12222.5 kN (V or Q from Str 1 to 4)

Do not include horizontal load from opposite battered piles in H_x and H_y below.

H_y = sum of horizontal loads in the Y direction = -2687.6 kN (H_{y1} from Str 1 to 4)

H_x = sum of horizontal loads in the X direction = 456.0 kN

H_x is the sum of F_{hx} (component of F_h plus Additional transverse F_{hx} from Input worksheet)

Note: Starting point used for lever arm length for M_{x1} and M_{y1} should correspond with point for "dist. from axis" for pile layout data.

M_{y1} = Y direction moments about X axis from gravity lds. = 14628.1 kN.m (M_{ry} from Str 1 to 4)

M_{x1} = X direction moments about Y axis from gravity lds. = 211357.9 kN.m (M_{rx} from Str 1 to 4)

M_{y2} = Y direction moments about X axis from horiz. lds. = -4381.8 kN.m (M_{oy} from Str 1 to 4)

M_{x2} = X direction moments about Y axis from horiz. lds. = 0.0 kN.m (M_{ox} from Str 1 to 4)

M_{x3} = additional moments in X direction about mid-length of footing = 1204.4 kN.m

$M_y = M_{y1} + M_{y2}$ = sum of moments in the Y direction about X axis = 10246.3 kN.m

$M_{x1_x2} = M_{x1} + M_{x2}$ = sum of moments in the X direction about Y axis = 211357.9 kN.m

d_y = distance to centroid of load from the X axis = M_y / V = 0.838 m

d_x = distance to centroid of load from the Y axis = M_{x1_x2} / V = 17.293 m

Torsion - Clockwise:

T_y = torsional moments from H_y = 0.0 kN.m

T_x = torsional moments from H_x = 0.0 kN.m

Torsion - Counterclockwise:

T_y = torsional moments from H_y = 0.0 kN.m

T_x = torsional moments from H_x = -239.4 kN.m

Design of Pile 1:

| | | | |
|---|---------------------------------------|--------------------------|---------------|
| <u>Single Pile Design</u> | Pile I.D.: | 1 | (1 to 86) * |
| <u>DATA</u> | Note: all piles to act in compression | | |
| Allowable Compression Load on Vertical Piles = | 620.0 | kN | |
| Allowable Compression Load on Battered Piles = | 620.0 | kN | |
| Is pile battered in Y direction | Yes | | |
| Batter of pile = | 3.0 | vertical to 1 horizontal | |
| Is pile battered in X direction | No | | |
| Batter of pile = | 0.0 | vertical to 1 horizontal | |
| <u>GRAVITY LOAD EFFECTS:</u> | | | |
| Vert. ld / pile = gravity ld on a pile + $\frac{\sum M_y' \text{ and } M_x' \text{ about the c.g of piles } * c_y \text{ and } c_x}{\text{Inertia ' y ' and Inertia ' x '}}$ | | | |
| -gravity ld may be the total ld / N ^o of piles if the structure is considered rigid such as a bridge abutment or the gravity ld shall be determined per pile based on the ld from the contributing area. | | | |
| gravity load from V per pile = v = | 407.4 | kN | |
| y' = distance from X axis to pile = | 0.350 | m | |
| x' = distance from Y axis to pile = | 2.000 | m | |
| M _y ' = moment in Y direction = V * (d _y - y') = | -916.9 | kN.m | |
| M _x ' = moment in X direction = V * (d _x - x') = | -10557.5 | kN.m | |
| c _y = dist from c.g. of piles to design pile = | -0.563 | m | |
| c _x = dist from c.g. of piles to design pile = | -16.156 | m | |
| v _y = Vertical ld / pile in Y direction (excl. gravity) = | 41.5 | kN | |
| v _x = Vertical ld / pile in X direction (excl. gravity) = | 54.7 | kN | |
| d _x = dist from M _{x3} to pile ' x ' = | -15.293 | m | |
| Vertical ld / pile ' x ' from M _{x3} = v _{x3} = | -5.9 | kN | |
| Vertical Load in Pile = v + v _y + v _x + v _{x3} = | 497.7 | kN | |
| Horizontal component / pile in Y direction from Vertical ld. = | 165.9 | kN | |
| Horizontal component / pile in X direction from Vertical ld. = | 0.0 | kN | |

TORSION DATA:

c_{1y} = dist from c.g. of battered piles from Y axis to battered pile along x axis = 16.295 m
 c_{1x} = dist from c.g. of battered piles from X axis to battered pile along y axis = 1.300 m
 c = straight line dist from c.g. of battered piles to battered pile = 16.346 m

 Applicable J = 2268.77 m²
 Horizontal component / pile from Torsion Id. = -1.7 kN
 Include Torsion Id. in further design Yes

AXIAL DESIGN CHECK:

Axial Force in Pile = 524.6 kN < compr. resist of pile, therefore OK

HORIZONTAL STABILITY:

Manually tabulate individual results below onto Design 3 to determine overall stability of entire substructure.

Horizontal Stability Check of battered pile in Y direction:

Horizontal component / pile in Y direction = 165.9 kN from vertical loads
 Passive resistance of pile in Y direction = kN
 Structural resistance (assumed fixed at a depth) = kN
 165.9 kN (H_y resistance)

Percentage of H_y loading pile = 4.35 %
 Horizontal force / battered pile 'y' from H_y = 116.9 kN
 Total including Horizontal component / pile from Torsion Id. = 115.1 kN (H_y loading)

165.9 kN >= 115.1 kN **therefore OK**

Horizontal Stability Check of battered pile in X direction:

Horizontal component / pile in X direction = 0.0 kN from vertical loads
 Passive resistance of pile in X direction = kN
 Structural resistance (assumed fixed at a depth) = kN
 0.0 kN (H_x resistance)

Percentage of H_x loading pile = 0.00 %
 Does pile act in compression to resist H_x : Yes **drop down list**
 Horizontal force / battered pile 'x' from H_x = 0.0 kN
 Total including Horizontal component / pile from Torsion Id. = 0.0 kN (H_x loading)

0.0 kN >= 0.0 kN **therefore OK**